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Optimal PID Controller Based on Different Modified Grasshopper Optimization Algorithm for Nonlinear

Single-Input Single-Output System

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ABSTRACT

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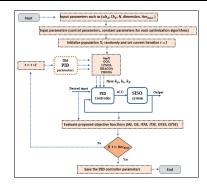
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This paper presents a comparative study of the Grasshopper Optimization Algorithm (GOA) with three suggested modified versions—Levy Flight GOA (LFGOA), Dynamic Attraction-Repulsion GOA (DARGOA), and Chaotic GOA (CHGOA)—for tuning Proportional-Integral-Derivative (PID) controller parameters in a nonlinear Single-Input Single-Output (SISO) system. The research contribution is the development and evaluation of CHGOA, which aims to improve convergence speed and transient response stability. The methodology employs exploratory and exploitative mechanisms of each algorithm to optimize PID parameters based on six objective functions. Performance metrics include rise time, settling time, overshoot, peak value, and best fitness obtained from MATLAB/Simulink simulations. A secondorder Mass-Spring-Damper (MSD) system is used as a representative nonlinear SISO system. Simulation results indicate that the proposed CHGOA consistently achieves lower fitness values, faster convergence, and stable transient responses compared to LFGOA, DARGOA, and standard GOA, under the tested objective functions. While LFGOA and DARGOA show competitive performance in traditional error metrics, standard GOA exhibits slower convergence in simulation scenarios. In this paper, the performance of the MSD system controlled by the proposed optimal PID with GOAs was also compared with the performance of this system with Nonlinear PIDs (NPIDs) which proposed by previous studies. The comparison results showed the efficiency of our proposed controllers in improving the performance of the MSD system, especially the CHGOA. Overall, the proposed CHGOA provides an effective balance between error minimization, convergence speed, and transient response performance, making it suitable for high-precision realtime applications.

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1. INTRODUCTION

The nonlinear Single-Input Single-Output (SISO) systems represent a significant challenge in control engineering due to their inherent complexity and the difficulty of modeling them accurately using conventional techniques. Such systems exhibit nonlinear behaviors that limit the effectiveness of classical linear control methods. These systems appear in many industrial and engineering applications, including the control of electric motors, mechanical systems with nonlinear friction, and aerodynamic processes.

Generally, nonlinear SISO systems are addressed through two main approaches: linear approximation and nonlinear control. In some cases, the system can be linearized around a specific operating point, enabling the application of established techniques such as Model Predictive Control (MPC) [1]–[3], Linear Quadratic Gaussian (LQG) [4][5], and Proportional-Integral-Derivative (PID) control [6][7]. However, when the system exhibits strong nonlinearities or requires operation across a wide range of conditions, more advanced control methods are necessary. These include Model Reference Control (MRC) with Fuzzy Logic [8][9] and adaptive Sliding Mode Control (SMC) [10]–[12], which offer enhanced robustness and better handling of unexpected disturbances and parameter variations.

Optimization techniques have become fundamental tools for finding optimal controller parameters to improve system performance, minimize error, and ensure stability. In particular, metaheuristic algorithms have gained increasing attention due to their capability to automatically tune controller parameters for nonlinear SISO systems, especially PID controllers. For example, Praveen Kumar et al. [13] introduced a PID controller design based on the Cuckoo Optimization Algorithm (COA), successfully applied to nonlinear systems such as the inverted pendulum, ship roll dynamics, and the Van der Pol Oscillator (VDPO). Hazem I. Ali et al. [14] designed an optimal nonlinear controller based on the model reference approach, optimized with the Invasive Weed Optimization (IWO) algorithm, and validated on the ball and plate system, showing improved robustness and performance. However, conventional metaheuristic algorithms may suffer from limitations such as slow convergence, premature entrapment in local optima, and an insufficient balance between exploration and exploitation [15]-[17]. To overcome these limitations, several algorithmic enhancements have been proposed. Vishal Srivastava et al. [18] introduced hybrid optimization approaches by integrating Particle Swarm Optimization with the Gravitational Search Algorithm (PSO-GSA) and with the Grey Wolf Optimizer (PSO-GWO) for tuning PID controllers in nonlinear systems such as the Continuous Stirred Tank Reactor (CSTR), inverted pendulum, and blood glucose regulation models. Vijayakumar Kaliappan [19] developed an Enhanced Genetic Algorithm (EGA)-based PID controller to regulate nonlinear closed-loop CSTR systems, demonstrating improved performance over conventional approaches through simulation. Furthermore, Zijing Chu et al. [20] presented a novel PID tuning approach integrating Whale Optimization Algorithm (WOA) with Backpropagation (BP) neural networks for nonlinear and time-varying problems, achieving fast response, improved stability, reduced overshoot, and high control precision. The Grasshopper Optimization Algorithm (GOA), inspired by grasshopper swarming behavior, has been enhanced through the integration of Lévy flight mechanisms into its structure, leading to the development of the Lévy Flight GOA (LFGOA), which improves global exploration, accelerates convergence, and enhances solution accuracy in engineering optimization problems [21][22]. Furthermore, the combination of chaotic maps with swarm-based optimizers has demonstrated robust performance improvements. For instance, a hybrid Particle Swarm Optimization-Gravitational Search Algorithm (PSO-GSA) incorporating chaotic mapping achieved superior robustness in $H_2/H\infty$ control design for generator-based systems [23].

This study builds upon these insights by proposing three modified variants of GOA that incorporate Lévy Flight GOA (LFGOA), Chaotic (CHGOA), and Dynamic Attraction-Repulsion (DARGOA). both the original and the improved variants of the GOA are employed to tune the PID controller parameters to enhance convergence speed, superior stability, robustness, and control accuracy of nonlinear SISO system. in this paper a second order Mass-Spring Damper (MSD) was considerd as an example of SISO nonlinear system. The suggested optimization algorithms are initially evaluated using the CEC2017 benchmark functions to validate their optimization performance. The optimization process considers six objective functions. These functions allows for a comprehensive comparison between the original and the modified GOA versions, highlighting the improvements achieved through algorithmic modifications.

The rest of this paper is organized as follows, the origin GOA and the suggested modified GOAs are given in section 2, the fitness function types are detailed in section 3, the Benchmark functions (CEC2017) are illustrated and performance analysis in Section 4, designing an optimal PID controller for nonlinear SISO system is explained in Section 5, the simulation results and analysis are shown in Section 6, and the conclusions are presented in Section 7.

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GRASSHOPPER OPTIMIZATION ALGORITHM AND SUGGESTED MODIFICATION 2. **METHODS**

Optimization refers to the process of determining the best solution to a given problem by improving the characteristics of a cost function and achieving the global optimum. Population-based, or metaheuristic, optimization methods are stochastic approaches that explore the search space through multiple candidate solutions (agents). Many of these stochastic strategies are inspired by natural phenomena, where the collective behaviors of animals and insects such as birds, ants, grasshoppers, flies, and even microorganisms are modeled, and are therefore categorized as Nature-Inspired Algorithms. One of the optimization algorithms techniques is Grasshopper Optimization Algorithm. This method is introduced by Saremi et al. [24], a novel and intriguing swarm intelligence technique that mimics the foraging and swarming behavior of grasshoppers. These insects significantly impact crop production and agriculture [25][26]. The mathematical modeling of this behavior is expressed through the position update mechanism represented in Eq. (1), which defines how grasshoppers interact and adjust their positions based on social forces and environmental influences.

$$X^{d}_{i} = c \left(\sum_{\substack{j=1\\j\neq i}}^{n} c \frac{ub_{d} - lb_{d}}{2} s(|x^{d}_{j} - x^{d}_{i}|) \frac{x_{j} - x_{i}}{d_{ji}} \right) + \hat{T}_{d}$$
 (1)

 $d_{ji} = |x^d_j - x^d_i| = r$ is distance between two grasshoppers i^{th} and j^{th} , s(r) is social force function computed as follows:

$$s(r) = Fe^{\frac{-d}{l}} - e^{-d} \tag{2}$$

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As expressed in above equation, the position of the i^{th} grasshopper at iteration t+1 denoted by $X_i(t+1)$ is updated according to the interactions among individuals and the target position. In this formulation, F represents the strength of attraction between grasshoppers, while I defines the attraction length. The search boundaries for each dimension are limited by the lower and upper bounds, ub_d and lb_d . The term \hat{T}_d corresponds to the target location in the d-dimensional search space. Furthermore, the shrinking coefficient c is employed to gradually reduce the comfort zone, ensuring a balance between exploration and exploitation during the optimization process.

$$c = c^{max} - j \frac{c^{max} - c^{min}}{Iter_{max}}$$
 (3)

where c^{max} is the maximum value, c^{min} is the value of minimum, j is the current iteration, and $Iter_{max}$ indicates the maximum number of iterations.

The optimization process in GOA begins by initializing a set of candidate solutions, where each grasshopper's position corresponds to a design variable vector. During the search, these positions are iteratively updated according to Eq. (1) to Eq. (3), while the best-performing individual is continuously tracked. This evolutionary mechanism is repeated until the termination criterion is satisfied, at which point the position of the best grasshopper is considered the optimal solution. In the following subsections, the three suggested methods to modify the origin GOA are explained. These methods are Lévy Flight GOA (LFGOA), Dynamically Attraction-Repulsion GOA (DARGOA), and Chaotic GOA (CHGOA).

2.1. Modified Grasshopper Optimization Algorithm Based on Lévy Flight

Lévy flight [27] is a mathematical model that facilitates random search behavior with occasional long jumps, making it particularly effective for enhancing exploration in optimization algorithms. Due to the complexity of its exact implementation, an approximated simulation is used here as follows:

$$LevyF(d) = \frac{r_1 \times \sigma}{|r_2|^{\frac{1}{\beta}}} \tag{4}$$

Here, d denotes the problem dimension, while r_1 and r_2 are two uniformly distributed random variables within the interval [0, 1]. The parameter β is a constant set to 1.5 as suggested by S. Mirjalili [28], and σ is computed using the following expression:

$$\sigma = \left(\frac{\Gamma(1+\beta) \times \sin\left(\frac{\pi\beta}{2}\right)}{\Gamma\left(\frac{1+\beta}{2}\right) \times \beta \times 2^{\frac{\beta-1}{2}}}\right)^{1/\beta}$$
 (5)

where $\Gamma(x) = (x - 1)!$.

In this work, the original GOA is modified by incorporating the Lévy Flight mechanism directly into the core position update formula. Specifically, a subset of 50% of the search agents is guided to perform Lévy-based movements when no better neighboring solutions are identified. This adjustment aims to increase exploration capability and reduce the risk of premature convergence. Unlike prior works [29][30] where Lévy steps are often implemented as external modifications or separate random walks, the proposed modification applies the Lévy jump directly within the attraction-repulsion formula on Eq. (1). This integration enhances the algorithm's ability to escape local optima while maintaining a balance between diversification and intensification. The mathematical formulation of the Lévy jump is defined as follows:

$$X_{i}(IndexLevy) = X_{i}(IndexLevy) + LevyF(d)$$
(6)

where agents satisfying:

$$IndexLevy = rand(N, 1) < 0.5 \tag{7}$$

where *N* is number of agents are selected to undergo the Lévy-based update.

2.2. Modified Grasshopper Optimization Algorithm Based on Dynamically Attraction-Repulsion

In order to achieve a more effective trade-off between the exploration and exploitation phases within the GOA, a dynamic modification of the attraction (F) and repulsion (l) coefficients is introduced. Unlike the standard GOA in Eq. (2), which uses fixed values (F = 0.5 and l = 1.5) as proposed by S. Mirjalili in [28], this approach employs linearly time-varying parameters defined as follows:

$$F(t) = -((F_{max} - F_{min})/Iter_{max}) * t$$
(8)

$$l(t) = -((l_{max} - l_{min})/lter_{max}) * t$$
(9)

Where t is the current iteration and $Iter_{max}$ is the maximum number of iterations. The parameter ranges were selected based on both the original GOA constants and empirical testing:

- $F_{max} = 0.5$: consistent with the original GOA to ensure strong initial attraction
- F_{min} = 0.1: to gradually reduce inter-agent attraction near convergence.
- $l_{max} = 1.5$: default repulsion distance in the original model.
- $l_{min} = 0.5$: reduces the repulsion effect at later iterations for better convergence.

This modification is inspired by a recent study [31], which employed time-varying parameters to gradually reduce the interaction zone among agents, thereby improving convergence and limiting excessive exploration.

2.3. Modified Grasshopper Optimization Algorithm Based on Chaotic

To achieve a better trade-off between exploration and exploitation in the original GOA, the primary position update equation (Eq. (1)) is refined through the incorporation of a chaotic term based on the Logistic Map. The logistic map is a well-known nonlinear function that produces chaotic behavior and has been widely used to diversify search trajectories and avoid premature convergence [32], where logistic map equation is defined as follows:

$$chao f_{k+1} = \rho (1 - chao f_k) \tag{10}$$

where the control parameter ρ is assigned a value of 4 to ensure the generation of random numbers within the interval (0, 1) [32].

In this work, we directly embed the logistic value into the attraction-repulsion term of the position update formula, instead of using chaos for initial population or parameter control as done in prior works [33]. The

modified position update equation is given by:

$$X^{d}_{i} = c \left(\sum_{\substack{j=1\\j\neq i}}^{n} chaof * \left(c \frac{ub_{d} - lb_{d}}{2} s(|x^{d}_{j} - x^{d}_{i}|) \frac{x_{j} - x_{i}}{d_{ji}} \right) \right) + \hat{T}_{d}$$
(11)

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As illustrate in Eq. (11) subsections, the modification to the original GOA (LFGOA, DARGOA, and CHGOA) are suggested to address specific performance limitations, including premature convergence, imbalance between exploration and exploitation, and adaptation to complex search landscapes. To consolidate these enhancements and facilitate a direct step-by-step comparison with the baseline algorithm, all versions were reformulated into a unified pseudo-code framework. This integration not only standardizes the representation but also allows for clear identification of the operational differences between the original GOA and its variants. Specifically, Table 1 provides the complete modified unified pseudo-code, where the first column outlines the original GOA steps, and the following columns detail the corresponding modifications applied in LFGOA, DARGOA, and CHGOA.

Table 1. Unified Pseudo-code for Original GOA with Three Modifications

	Table 1. Unified Pseudo-code for Original GOA with Three Modifications.									
Step	Original GOA	LFGOA (GOA + Lévy flight)	DARGOA (Adaptive F & l)	CHGOA (Logistic Map)	Remark					
1	Initialize population X_i randomly within $[ub_a, lb_d]$, $i = 1N$	Same as Original	Same as Original	Same as Original	-					
2	Initialize parameters $F = 0.5$, $l = 1.5$, c^{max} , c^{min}	Same	Adapt F and l dynamically in Step 5.2	Same	Parameter adaptation in DARGOA					
3	Evaluate fitness $f_i = \text{fobj}(X_i)$	Same	Same	Same	-					
4	Set best solution $X_{best} = \min(f_i)$	Same	Same	Same	-					
5	While $j < Iter_{max}$:	Same	Same	Same	Iterative update loop					
5.1	Update shrinking factor: $c = c^{max} - j \frac{c^{max} - c^{min}}{Iter_{max}}$	Same	Same	Same	-					
5.2	Update positions: Eq. (1) with $s(r)$	Same + Lévy flight: $if \ rand(N, 1) < 0.5$ $X_i = X_i + LevyF(d)$	Adapt F and l dynamically $F(t) = -((F_{max} - F_{min})/lter_{max}) * t,$ $l(t)$ $= -((l_{max} - l_{min})/lter_{max}) * t$	Replace Eq. (1) to Eq. (11)	Main differences occur here					
5.3	Boundary check: $X_i \in [ub_d, lb_d]$	Same	Same	Same	-					
5.4	Evaluate fitness $f_i = \text{fobj}(X_i)$	Same	Same	Same	-					
5.5	Update best solution: if $f_i < f_{best}$: $X_{best} = X_i$, $f_{best} = f_i$	Same	Same	Same	-					
6	End While	Same	Same	Same	Termination condition met					

3. FITNESS FUNCTION TYPES

Designing any type of controller requires the determination of optimal control parameters. Accordingly, specific parameters must be calculated to minimize the chosen objective function. It is important to note that, since the system error is generally time-dependent, multiple performance indices are needed to comprehensively evaluate controller performance. Several fitness functions are widely employed in control optimization, including the Integral of Squared Time multiplied by Squared Error (ISTSE), Integral Squared Error (ISE), Integral of Squared Time multiplied by Error Squared (ISTES), Integral Absolute Error (IAE), Integral of Time multiplied by Squared Error (ITSE), and Integral of Time multiplied by Absolute Error (ITAE). The mathematical formulations of these performance indices are presented in the equations of these functions are [34]–[37]:

$$IAE = \int_{0}^{\infty} |e(t)| dt$$

$$ISE = \int_{0}^{\infty} e^{2}(t) dt$$
(12)

$$ISE = \int_{0}^{\infty} e^{2}(t)dt \tag{13}$$

$$ITAE = \int_{0}^{\infty} t |e(t)| dt$$
(14)

$$ITSE = \int_{0}^{\infty} te^{2}(t)dt$$

$$ISTES = \int_{0}^{\infty} |t^{2}e(t)|^{2} dt$$

$$ISTSE = \int_{0}^{\infty} t^{2}e^{2}(t)dt$$
(15)

$$ISTES = \int_{0}^{\infty} |t^2 e(t)|^2 dt \tag{16}$$

$$ISTSE = \int_{0}^{\infty} t^2 e^2(t) dt \tag{17}$$

PERFORMANCE ANALYSIS ON CEC2017 BENCHMARK FUNCTIONS AND **EVALUATION OF SUGGESTED METHODS**

The CEC2017 benchmark suite contains 23 functions, as detailed in Table A1 to Table A3 in Appendix A [38]. In these tables, (Range) denotes the search space boundaries, (D) represents the dimensionality of each function, and (V_{op}) indicates the known global optimum. All benchmark functions are formulated as minimization problems and are categorized into three types: unimodal functions (F1-F7), multimodal functions (F8–F13), and fixed-dimension multimodal functions (F14–F23) [33]. In the present study, to ensure a rigorous and fair comparison, each algorithm was executed 30 independent times on every benchmark function, with a population size of 50 and a maximum of 500 iterations. The performance of each algorithm was assessed by evaluating the mean and standard deviation of the obtained solutions, where lower values correspond to higher robustness and stability in achieving global optimization.

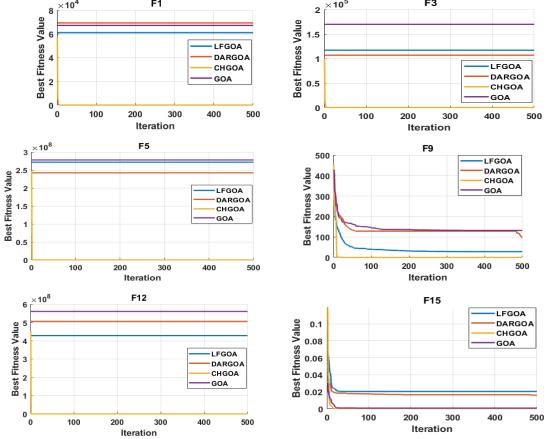
A series of experiments were conducted on a selected set of CEC2017 benchmark functions: F1, F3, F5, F9, F12, F15, F22, and F23. These functions were carefully chosen due to their diverse characteristics, including unimodal, multimodal, hybrid, and composition functions, providing a comprehensive and challenging environment to evaluate the algorithms exploration, exploitation, convergence speed, and solution accuracy capabilities. The performance evaluation involved the original GOA alongside three suggested enhancements: CHGOA, DARGOA, and LFGOA. These variants aim to improve the exploration-exploitation balance, enhance the quality of search in later stages, and reduce the likelihood of premature convergence to local optima. All experiments were conducted under uniform settings regarding population size, number of iterations, and independent runs to ensure a fair and reliable comparison. The results from the comparative performance Table 2 indicate that CHGOA outperforms other algorithms across most functions, especially complex multimodal ones such as F1, F3, and F5, achieving best values near the global optimum with low standard deviation, indicating high accuracy and consistent stability across runs. DARGOA ranks second overall, showing notable improvements over the baseline GOA by reducing mean and standard deviation values, reflecting greater reliability and steadiness. LFGOA demonstrated strong and stable performance particularly on complex composition functions like F22 and F23, attaining the best values and lowest ranks, which indicates its superior capability to explore intricate search spaces precisely. Conversely, the original GOA exhibited variable performance, often ranking in mid to lower positions, underscoring the necessity of the applied enhancements. Moreover, the convergence curves for each benchmark function are presented in Figure 1.

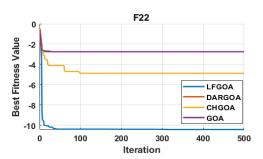
Table 2. Statistical results of benchmark functions for original GOA with three modifications.

Funct-ion	Algorithm	Best	Mean	Median	Worst	Std	Rank
	LFGOA	5.1597e+04	6.6415e+04	6.7461e+04	7.9099e+04	6.2309e+03	4
F1	DARGOA	4.0068e+04	6.2679e+04	6.2994e+04	7.2843e+04	6.9920e+03	2
	CHGOA	3.5531e-09	3.3045e-05	3.1548e-05	8.9628e-05	2.4074e-05	1
	GOA	4.6765e+04	6.3980e+04	6.4823e+04	7.5011e+04	7.0392e+03	3

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8 ^ 10				۵			
×10 ⁴		F1		2 ×10	5	F3	
	GOA	-10.5353	-6.6485	-5.1512	-2.4217	3.7845	3
1.77	CHGOA	-10.1022	-5.2489	-5.0077	-2.7597	1.2524	4
F23	DARGOA	-10.5354	-7.0533	-7.8201	-1.6758	3.6411	2
	LFGOA	-10.5355	-7.7665	-10.5289	-2.4216	3.7485	1
	GOA	-10.4023	-5.8027	-5.0864	-1.8376	3.2334	3
ΓΖΖ	CHGOA	-10.2162	-5.3139	-4.9705	-2.6177	1.5397	4
F22	DARGOA	-10.4010	-6.9423	-7.7272	-1.8360	3.5728	2
	LFGOA	-10.4024	-7.0453	-7.7596	-2.7516	3.5087	1
	GOA	3.0831e-04	0.0065	0.0015	0.0297	0.0093	2
F15	CHGOA	3.1152e-04	0.0018	3.2116e-04	0.0209	0.0052	1
F1.5	DARGOA	7.5883e-04	0.0139	0.0181	0.0594	0.0153	4
	LFGOA	4.3107e-04	0.0067	7.8390e-04	0.0565	0.0124	3
	GOA	1.8904e+08	5.0483e+08	5.1512e+08	7.4218e+08	1.2790e+08	4
F12	CHGOA	0.0521	0.1405	0.1317	0.3733	0.0654	1
E10	DARGOA	3.4466e+08	5.0375e+08	5.0111e+08	7.1863e+08	1.0722e+08	2
	LFGOA	2.5742e+08	5.0402e+08	5.1791e+08	6.9529e+08	1.2279e+08	3
	GOA	18.3995	73.8144	61.3623	201.3240	42.0337	3
F9	CHGOA	0.0038	0.0090	0.0091	0.0153	0.0026	1
F0	DARGOA	87.6969	170.3005	153.6646	299.6026	54.3970	4
	LFGOA	13.4004	69.3096	51.0655	233.3008	51.4547	2
	GOA	1.7801e+08	2.4519e+08	2.4757e+08	2.9968e+08	3.4426e+07	4
F5	CHGOA	28.7968	28.8659	28.8667	28.9126	0.0306	1
7.5	DARGOA	1.2700e+08	2.3000e+08	2.4119e+08	2.9766e+08	4.0783e+07	2
	LFGOA	1.5271e+08	2.3258e+08	2.3265e+08	2.9188e+08	3.6792e+07	3
	GOA	5.4643e+04	1.2786e+05	1.2869e+05	1.9218e+05	3.6305e+04	3
F3	CHGOA	2.4606e-07	1.1741e-04	1.2276e-04	2.6940e-04	6.8568e-05	1
	DARGOA	5.2373e+04	1.1605e+05	1.1570e+05	2.1691e+05	3.7302e+04	2
F3							





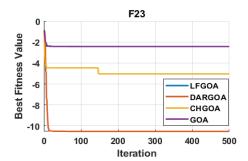


Figure 1. Convergence characteristics of the modified and baseline optimization algorithms on eight detailed benchmark functions

5. OPTIMAL PID CONTROLLER DESIGN FOR SISO NONLINEAR MSD SYSTEM

In this study, the Mass spring Damper (MSD) system is adopted as a representative nonlinear SISO plant to validate the effectiveness of optimization approaches for PID tuning by GOA and the modified GOA methods. The MSD system shown in Figure 2 is a mechanical standard benchmark in control theory for vibration dynamics, it can be described as follows [39][40]:

$$M\ddot{x} + g(x, \dot{x}) + f(x) = \emptyset(\dot{x})u(t) \tag{18}$$

The parameters of this system are listed in Table 3.

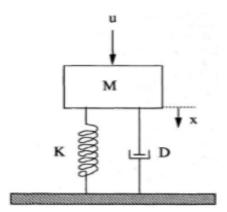


Figure 2. Nonlinear MSD system [40]

Table 3. Model parameters of MSD [40]

Symbol	Description	Value
M	mass	1.0
$g(x,\dot{x})$	the nonlinear or uncertain term with respect to the spring, $g(x,\dot{x}) = (d_1x + d_2\dot{x}^3)$	$d_1 = 0.01,$ $d_2 = 0.1$
f(x)	the nonlinear or uncertain term with respect to the damper, $f(x) = d_3x + d_4x^3$	$d_3 = 0.01,$ $d_4 = 0.67$
$\emptyset(\dot{x})$	the nonlinear term with respect to the input term $\phi(\dot{x}) = 1 + d_5 \dot{x}^3$	$d_5 = 0$
x	$\in [-a \ a], a > 0$	a = 1.5
х	\in [-b b], b > 0	b = 1.5
и	Force control signal	

Then, Eq. (18) can be rewritten as follows:

$$\ddot{x} = -0.1\dot{x}^3 - 0.02x - 0.67x^3 + u(t) \tag{19}$$

The state-space representation of the Eq. (19) is expressed as:

 $\dot{r}_{c} = r_{c}$

$$\dot{x}_1 = x_2
\dot{x}_2 = -0.1\dot{x}^3 - 0.02x - 0.67x^3 + u(t)
y = x_1$$
(20)

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The control law of the PID controller is given by:

$$u(t) = k_p e(t) + k_i \int e(t) dt + k_d \frac{de(t)}{dt}$$
(21)

where k_p , k_i , and k_d are the proportional, integral, and derivative gains, respectively. The six performance indices IAE, ISE, ISTES, ISTSE, ITAE, and ITSE are used as fitness functions to evaluate the quality of the PID tuning for MSD system.

Figure 3 provide a clearer understanding of the interaction between the optimal PID controller and the MSD system and illustrates the step-by-step procedure: starting with the initialization of control parameter bounds, followed by the configuration of the optimization algorithm settings, and finally the evaluation of the MSD system response under the optimized PID controller.

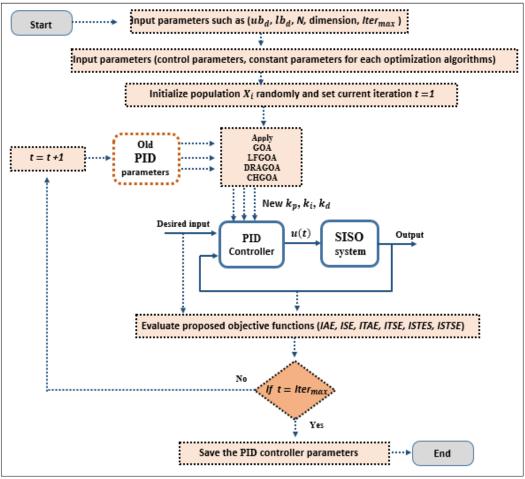


Figure 3. Flowchart of designing optimal PID tuned by modified GOAs for nonlinear MSD system

6. SIMULATION RESULT AND ANALYSIS

In this section, a comprehensive analysis is conducted on the performance of the SISO nonlinear MSD system regulated by a PID controller optimized by original GOA and the three suggested modified methods (LFGOA, DARGOA, and CHGOA). A series of simulation tests is carried out to evaluate and compare the effectiveness of each optimization approach in achieving precise and stable control performance. Unity step reference signal is assigned to ensure consistency across all trials. The system parameters adopted in the simulations are listed in Table 4, while Table 5 summarizes the PID controller parameters obtained by each algorithm to maintain the actual system output at the desired reference.

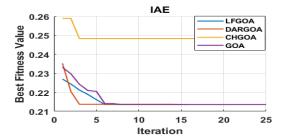
Figure 4 displays the convergence curves for selected benchmark functions, clearly showing the performance differences among the four algorithms, while the bar chart in Figure 5 provides a comparative view of the best fitness values obtained in PID tuning tasks. Across most fitness functions, CHGOA demonstrated a clear advantage in minimizing the best fitness values, as reflected in benchmark results such as F1, F3, F5, F9, F12, and F15, where it consistently achieved the top rank. On the other hand, GOA generally performed on par with LFGOA and DARGOA in basic error metrics but lagged behind in more complex benchmark functions (F1–F15), indicating a relatively slower convergence in highly nonlinear optimization landscapes. Nevertheless, GOA maintained consistent stability, which may be advantageous in systems with strict robustness requirements. The simulation results to evaluate the performance of the controlled nonlinear MSD system for linear and nonlinear desired input are illustrate in the following subsections

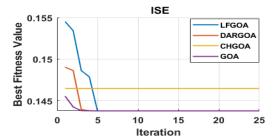
Table 4. Input parameters for optimization methods

Optimization methods	Parameters	Values
	dimension	3
	lower value for k_p , k_i , k_d	[40,2,8]
All	upper value for k_p , k_i , k_d	[50,6,12]
	Iter _{max}	25
	number of populations	25
GOA	intensity of attraction (f) , attractive length scale (l)	0.5, 1.5
LFGOA	r_1 , r_2 are random numbers in [0,1], $\beta = 1.5$	
DARGOA	$F_{max} = 0.5, F_{min} = 0.1, l_{max} = 1.5, l_{min} = 0.5$	
CHGOA	$\rho = 4, x_0 = 0.1$	

Table 5. Optimal PID parameters obtained by the optimization methods

Algorithm	Fitness	k_p	k_i	k_d
	IAE	50.0	4.73047	8.0
	ISE	50.0	5.25694	8.0
LFGOA	ISTES	48.373956	4.16773	9.024699
LFGOA	ISTSE	50.0	4.6764	8.0
	ITAE	44.564026	3.88562	9.018161
	ITSE	50.0	4.6726	8.0
	IAE	50.0	4.7175	8.0
	ISE	50.0	5.25817	8.0
DARGOA	ISTES	46.140447	4.1927	8.524579
DARGOA	ISTSE	50.0	4.67561	8.0
	ITAE	42.24318	3.84446	8.639904
	ITSE	50.0	4.69303	8.0
	IAE	40.0	3.69246	8.0
	ISE	49.085259	5.66306	8.280854
CHGOA	ISTES	42.994004	3.24590	10.424872
CHOOA	ISTSE	46.378976	3.76078	9.023849
	ITAE	40.0	3.90348	8.0
	ITSE	49.805628	2.38151	8.198259
	IAE	50.0	4.71757	8.0
	ISE	50.0	5.27205	8.0
GOA	ISTES	44.654183	3.67562	9.640629
GOA	ISTSE	50.0	4.71293	8.0
	ITAE	48.102895	3.94440	9.63532
	ITSE	50.0	4.65258	8.0





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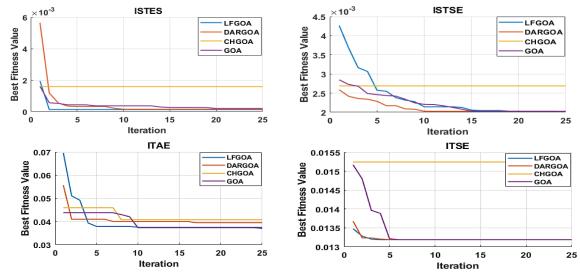


Figure 4. Convergence curves of six-fitness function types (IAE, ISE, ISTES, ISTSE, ITAE, ITSE) for different iteration numbers GOA, LFGOA, DARGOA, and CHGOA

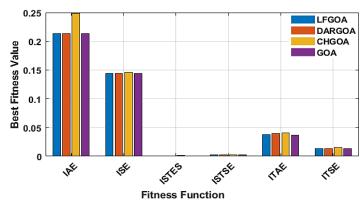


Figure 5. Bar chart illustrating the best fitness values for seven fitness functions obtained using GOA, LFGOA, DARGOA, and CHGOA

6.1. Simulation Results for Linear Desired Input

According to ISTES function and linear desired input (r(t) = 1), the simulation result (output position and control signal) of the controlled MSD based on optimal PID with (GOA, LFGOA, DARGOA, and CHGOA) are shown in Figure 6. These results shows that the actual output of the MSD follow the desired linear input faster with demonstrating stable behavior with variations in settling time, overshoot and error close to zero, where CHGOA exhibited the lowest overshoot.

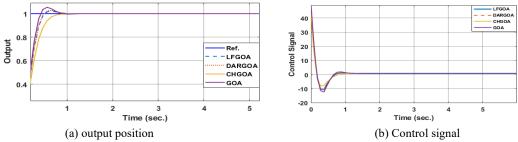


Figure 6. Response of MSD system for linear desired input controlled by optimal PID with different GOAs

Table 6 presents the time-domain performance results (rise time (t_r) , settling time (t_s) , overshoot (MOS %), peak value, and best fitness values) obtained from MATLAB/Simulink simulations. These results are evaluated using the six fitness functions (IAE, ISE, ISTES, ISTSE, ITAE, and ITSE) in the simulation

environment, each emphasizing different aspects of error minimization and transient performance. The practical time-domain results in Table 6 closely align with the benchmark-based outcomes in Table 2. Specifically, CHGOA consistently achieved top ranks and the lowest best fitness values across multiple CEC2017 functions (F1, F3, F5, F9, F12, F15), which correlates with its ability to eliminate overshoot in ISTES and ITAE, despite a slightly longer t_r . LFGOA and DARGOA also exhibited strong performance in specific benchmark functions (F22 and F23), translating to faster t_s and reduced peak responses in PID control simulations.

Table 6 Comparison	of time response n	natrice for GOA	and modified GOAs	across multiple fitness functions

PID based on	Fitness	Rise time	Settling time (t_s) sec.	Peak	MOS%	Best Fitness	
		(t_r) sec.		Value			
	IAE	0.2786	0.7515	1.1	5.18	0.21358	
	ISE	0.2778	0.7637	1.1	5.37	0.14376	
LFGOA	ISTES	0.3163	0.4756	1.0	1.95	0.00013	
LIGOA	ISTSE	0.2787	0.7502	1.1	5.16	0.00203	
	ITAE	0.3376	0.5145	1.0	1.42	0.03749	
	ITSE	0.2787	0.7501	1.1	5.16	0.01319	
	IAE	0.2787	0.7512	1.1	5.18	0.21358	
	ISE	0.2778	0.7637	1.1	5.37	0.14376	
DARGOA	ISTES	0.3161	0.7447	1.0	2.86	0.00014	
DARGOA	ISTSE	0.2787	0.7502	1.1	5.16	0.00203	
	ITAE	0.3429	0.5176	1.0	1.66	0.03944	
	ITSE	0.2787	0.7506	1.1	5.17	0.01319	
	IAE	0.3401	0.7831	1.0	2.69	0.24828	
	ISE	0.2913	0.7822	1.0	4.48	0.14646	
CHCOA	ISTES	0.4211	0.7057	1.0	0.0	0.00159	
CHGOA	ISTSE	0.3276	0.495	1.0	1.56	0.00269	
	ITAE	0.3396	0.7952	1.0	2.8	0.04073	
	ITSE	0.29	0.6968	1.0	3.46	0.01524	
	IAE	0.2787	0.7512	1.1	5.18	0.21358	
	ISE	0.2778	0.764	1.1	5.38	0.14376	
CO.4	ISTES	0.3699	0.5753	1.0	0.5	0.00019	
GOA	ISTSE	0.2787	0.751	1.1	5.18	0.00202	
	ITAE	0.3414	0.5284	1.0	0.92	0.03700	
	ITSE	0.2787	0.7496	1.1	5.16	0.01319	

The results of Figure 6 and Table 6 indicate that LFGOA achieved the best overall performance in the ISTES criterion, with the lowest best fitness value, a short t_r and a fast t_s while maintaining a reduced maximum overshoot. DARGOA produced a similar ISTES performance with nearly identical t_r but a slightly higher overshoot. CHGOA, on the other hand, reached a best fitness of 0.001586 with t_s of 0.7057 sec., demonstrated the no overshoot for ISTES, albeit with a longer t_r (0.4211 sec.). The original GOA showed stable performance but was outperformed by some modifications in certain criteria, with its best ISTES value at 0.000194, with t_r 0.3699 sec., and MOS 0.5%. LFGOA and DARGOA exhibited competitive performance in classical error criteria such as IAE and ISE, with nearly identical t_r and t_s times. However, LFGOA consistently provided slightly lower overshoot and better fitness in certain benchmark functions (F22 and F23), making it favorable in scenarios where minimal overshoot and robustness to disturbance are prioritized. Although LFGOA shows slightly better performance in some individual PID metrics (e.g., ISTES), CHGOA consistently outperforms all algorithms across the CEC2017 benchmark functions and maintains a balanced performance in PID metrics, including fitness, rise time, settling time, and MOS%. Therefore, considering both benchmark and PID results, and based on this comprehensive set of performance criteria, CHGOA is regarded as the overall best algorithm.

6.2. Simulation Results for Nonlinear Desired Input

The simulation result (output position and control signal) of the controlled MSD based on optimal PID with (GOA, LFGOA, DARGOA, and CHGOA) for nonlinear $(r(t) = \sin(2t))$ desired input and ISTES function are shown in Figure 7. Table 7 presents the time-domain performance results of the best ISTES fitness function. The results of Figure 7 and Table 7 shows that the performance of the controlled MSD follow the desired nonlinear input faster with error close to zero and minimum ISTES spatially with CHGOA. Overall, the results indicate that while LFGOA and DARGOA are strong choices for conventional performance measures, CHGOA offers the most balanced trade-off between error minimization, convergence rate, and transient performance.

Figure 7. Response of MSD system for nonlinear desired input controlled by optimal PID with different GOAs

Table 7. Comparison of time-response fitness functions for GOA and modified GOAs

Optimization	LFGOA	DARGOA	CHGOA	GOA
ISTES	18.54	20.73	14.25	17.39

6.3. Comparison the results of our optimal PID based on GOAs with results of NPID of Refs. [40][41]

In this subsection, with desired input r(t) = 0.1, the performance of the nonlinear MSD model (Eq. (20) and parameters of Table 3) which is controlled by our suggested optimal PID based on GOAs are also compared with its performance based on two previous proposed modified Nonlinear PID. The first controller is NPID based on modified Han Tracking Differentiator (TD) [41], while the second controller is NPID based on Improved Nonlinear Tracking Differentiator (INTD) with hyperbolic tangent function proposed by Wameedh A. [40]. The simulation results (positions and control signal) for controlled MSD are shown in Figure 8 to Figure 10. A comparative performance analysis reveals that the proposed controllers achieve faster settling times compared to both Han and Wameedh methods, even though minor oscillations are observed in certain responses. Nevertheless, all proposed controllers maintain a zero steady-state error, confirming their superior tracking accuracy and stability. Furthermore, the control signal in Han's and Wameedh's methods starts approximately from a value of 2, whereas in the proposed methods it starts around 4, indicating a faster transient response. In addition, Han's controller exhibits noticeable jittering in the control signal, which may induce actuator vibration and undesired fluctuations. In contrast, the suggested optimal PID based on GOAs produce a smoother control signal, ensuring more stable actuation and improved overall system performance.

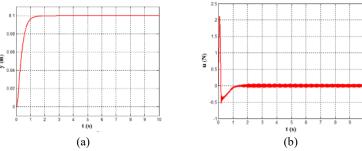


Figure 8. The simulation results of MSD controlled by NPID based on modified Han TD, (a)The control signal u, (b) The plant output y

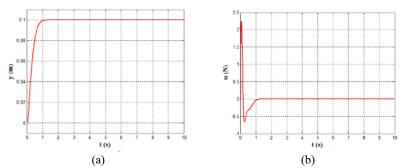


Figure 9. The simulation results of MSD controlled by NPID based on proposed Wameedh INTD, (a) The control signal u (b) The plant output y

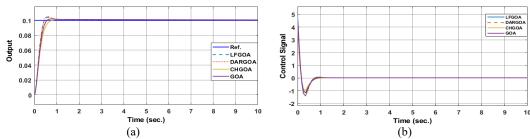


Figure 10. The simulation results of MSD controlled by optimal PID based on different GOAs, (a) The control signal u
(b) The plant output y

7. CONCLUSIONS

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This paper investigated GOA and three modified GOAs (LFGOA, DARGOA, and CHGOA) to tune the parameters of PID controller which is used to control a SISO nonlinear system. In this paper, a second order MSD is considered as example of SISO nonlinear system. A comprehensive comparison was conducted among the various GOAs. Based on the analysis of best fitness values, rise time, and settling time, the superior performance of CHGOA is evident compared to the other algorithms specifically targeting the reduction of the ISTES objective. Our results confirm that applying the suggested CHGOA achieves better precision tracking and transient stability than LFGOA, DARGOA, and GOA. Therefore, it is recommended to utilize CHGOA for tuning PID, with the ISTES fitness function forming its evaluation basis. Competing algorithms, such as LFGOA and DARGOA, can still enhance system performance in specific scenarios, particularly when minimizing overshoot and ensuring robustness against disturbances are priorities. Future work can expand this research in several directions to further enhance the effectiveness of PID optimization algorithms for the second order and higher order nonlinear SISO system and the potential directions can be include:

- Developing hybrid algorithms combining CHGOA with specific techniques like PSO or AOA, integrating
 advanced strategies such as Levy Flight or Opposition-based Learning to improve convergence speed and
 solution accuracy.
- 2. Exploring more advanced controller types, such as FOPID or Fuzzy PID, and comparing them with conventional controllers to enhance real-time control of nonlinear systems.
- 3. Adopting multi-objective optimization to minimize multiple performance metrics simultaneously, such as settling error, rise time, and overshoot, while providing Pareto-optimal solutions

DECLARATION

Author contribution

Aliaa A. Flaih: Original draft preparation, Formal analysis, Investigation, Software; Ekhlas H. Karam: Manuscript writing and review, Validation of results, Investigation, Yousra A. Mohammed: Investigation, Formal analysis and Validation of results.

Conflict of interest

The authors have no conflict of interest to declare.

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Appendix A

Table A1. Unimodal benchmark functions.

Function	Range	D	Vop
$f_1(y) = \sum_{i=1}^n y_i^2$	[-100,100]	30	0
$f_2(y) = \sum_{i=1}^n y_i + \prod_{i=1}^n y_i $	[-10,100]	30	0
$f_3(y) = \sum_{i=1}^{n} (\sum_{j=1}^{i} y_j)^2$	[-100,100]	30	0
$f_4(y) = max_i[y_i , 1 \le i \le n]$	[-100,100]	30	0
$f_5(y) = \sum_{i=1}^{n-1} \left\{ 100(y_{i+1} - y_i^2)^2 + (y_i - 1)^2 \right\}$	[-30,30]	30	0
$f_6(y) = \sum_{i=1}^n (y_i + 0.5)^2$	[-100,100]	30	0
$f_7(y) = \sum_{i=1}^{n} i y_i^4 + random(0,1)$	[-1.28,1.28]	30	0

Table A2. Multimodal benchmark functions

Function	Range	D	$V_{\rm op}$
f_8 (y)= $\sum_{i=1}^n -y_i \sin(\sqrt{ y_i })$	[-500,500]	30	-12569.5
$f_9(y) = \sum_{i=1}^{n} [y_i^2 - 10\cos(2\pi y_i) + 10]$	[-5.12,5.12]	30	0
f_{10} (y)=-20 exp $\left(-0.2\sqrt{\frac{1}{n}\sum_{i=1}^{n}y_{i}^{2}}\right)$	[-32,32]	30	0

$$-exp\left(\frac{1}{n}\sum_{i=1}^{n}\cos\left(2\pi y_{i}\right)\right)+20+e$$

$$f_{11}\left(y\right)=\frac{1}{4000}\sum_{i=1}^{n}y_{i}^{2}-\prod_{i=1}^{n}\cos\left(\frac{y_{i}}{\sqrt{i}}\right)+1 \qquad \left[-600,600\right] \quad 30 \qquad 0$$

$$f_{12}\left(y\right)=\frac{\pi}{n}\left\{10sin(\pi x_{1})+\sum_{i=1}^{n-1}(x_{i}-1)^{2}[1+10sin^{2}(\pi x_{i+1})]+(x_{n}-1)^{2}\right\}+\sum_{i=1}^{n}u(y_{i},10,100,4)$$

$$x_{i}=1+\frac{y_{i}+1}{4} \qquad \left[-50,50\right] \quad 30 \qquad 0$$

$$u(y_{i},k,a,m)=\begin{cases} k(y_{i}-a)^{m}\;;\;y_{i}>a\\0\;;\;-a< y_{i}

$$f_{13}\left(y\right)=0.1\left\{sin^{2}(3\pi y_{1})+\sum_{i=1}^{n}(y_{i}-1)^{2}[1+sin^{2}(3\pi y_{i}+1)]+(y_{n}-1)^{2}[1+sin^{2}(2\pi y_{n})]\right\}+\sum_{i=1}^{n}u(y_{i},5,100,4) \qquad \left[-50,50\right] \quad 30 \qquad 0$$$$

Table A3. Fixed-dimension multimodal benchmark functions

Function	Range	D	V _{op}
$f_{14} (y) = \left(\frac{1}{500} + \sum_{j=1}^{25} \frac{1}{j + \sum_{i=1}^{2} (y_i - a_{ij})^6}\right)^{-1}$	[-65,65]	2	1
$f_{15}(y) = \sum_{i=1}^{11} \left(a_i - \frac{y_1(b_i^2 + b_1 y_2)}{b_i^2 + b_1 y_3 + y_4} \right)^2$	[-5,5]	4	0.00030
f_{16} (y)=4 y_1^2 - 2.1 y_1^4 + $\frac{1}{3}y_1^6$ + y_1y_2 - 4 y_2^2 + 4 y_2^4	[-5,5]	2	-1.0316
f_{17} (y)= $\left\{y_2 - \frac{5.1}{4\pi^2}y_1^2 + \frac{5}{\pi}y_1 - 6\right\}^2 + 10\left(1 - \frac{1}{8\pi}\right)\cos y_1 + 10$	[-5,5]	2	0.398
$f_{18} (y) = [1 + (y_1 + y_2 + 1)^2 (19 - 14y_1 + 3y_1^2 - 14y_2 + 6y_1y_2 + 3y_2^2)] \times [30 + (2y_1 - 3y_2)^2 \times (18 - 32y_1 + 12y_1^2 + 48y_2 - 36y_1y_2 + 27y_2^2)]$	[-2,2]	2	3
$f_{19} (y) = -\sum_{i=1}^{4} c_i \exp \left(-\sum_{j=1}^{3} a_{ij} (y_j - p_{ij})^2\right)$	[1,3]	3	-3.86
$f_{20} (y) = -\sum_{i=1}^{4} c_i \exp \left(-\sum_{j=1}^{6} a_{ij} (y_j - p_{ij})^2\right)$	[0,1]	6	-3.32
$f_{21}(y) = -\sum_{i=1}^{5} [(Y - a_i)(Y - a_i)^T + c_i]^{-1}$	[0,10]	4	-10.1532
$f_{22}(y) = -\sum_{i=1}^{7} [(Y - a_i)(Y - a_i)^T + c_i]^{-1}$	[0,10]	4	-10.4028
$f_{23}(y) = -\sum_{i=1}^{10} [(Y - a_i)(Y - a_i)^T + c_i]^{-1}$	[0,10]	4	-10.5363

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