

# Adaptive FLC-based Shunt Active Power Filter with a PV-Fed DC Link for Improved Current Compensation and THD Mitigation

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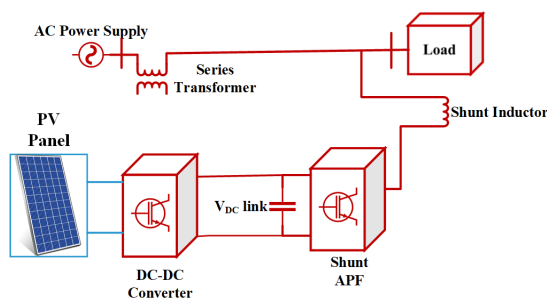
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## ABSTRACT



Power quality improvement with traditional controllers (PI, PID, fixed-parameter FLC) is difficult when dealing with nonlinear, time-varying loads and dynamic grid conditions. For microgrids that incorporate renewable energy sources, it is challenging to acquire the precise mathematical models that are necessary for this work. To address power quality challenges, such as distortion of current and Total Harmonic Distortion (THD), produced by nonlinear loads in PV fed systems, such as solar energy conversion, this publication proposes an Adaptive Fuzzy Logic Controller (FLC) based shunt Active Power Filter (APF). An analysis of the power quality enhancement achieved in a distribution power system using a single-stage solar PV integrated shunt APF is presented in this paper. In order to improve load side parameters, such as the elimination of even and odd current harmonics utilizing shunt APF is employed. This filter makes use of a shared DC-link voltage source. In addition, it transfers energy from the PV system's solar panels to the DC link voltage, which is an extra effort. In this paper, It looks at a single-phase inverter that uses an Adaptive FLC to improve parameters on the source and load sides, as well as harmonics, in grid-connected Distributed Generation systems. Also included is a detailed description of the active power filter's chosen current reference generator. Results that have been validated are attained using MATLAB/SIMULINK(R2023b).

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## 1. INTRODUCTION

When it comes to power sources, electrical energy has recently surpassed all others. Having access to power is fundamental to daily life. The dependability and regularity of the electricity supplied to the end user's apparatus are also critical to its efficient operation. A constant, high-quality power supply is commonly required by commercial and industrial loads [1]-[4]. That is why protecting the stability of the power grid must be an urgent concern. The nonlinear components have a significant impact on the power supply's efficiency and reliability [5]-[7]. Electronic equipment can lead to a range of power quality issues. Unreliable power might be caused by fluctuations in voltage that occur as a result of things like lightning strikes, network outages, or the switching of capacitor banks [8]-[12]. Overuse of rectifiers, laser printers, and computers results in reactive and harmonic power [12]-[14]. Immediate action is required to resolve this type of issue before it worsens. Despite their size, resonance issues, and the impact of the source impedance on performance, passive filters have traditionally been employed for reactive power disturbances and harmonic production. The energy supply can be made better with the help of active power filters [15]. In this paper, the shunt APF is controlled by the current in the d-q axes of the load current, and an adaptive FLC maintains the voltage at the Solar Fed DC-interface in Figure 1 [16]. Various load currents and variable voltage scenarios are covered in this work, along with the static and dynamic behavior of control circuits. With static and dynamic nonlinear loads, the Shunt APF is used to decrease fluctuations and harmonics, among other things, and an adaptable FLC is constructed for the plant as its parameters change. Power quality improvement with traditional controllers (PI, PID, fixed-parameter FLC) is difficult when dealing with nonlinear, time-varying loads and dynamic grid conditions. For microgrids that incorporate renewable energy sources, it is challenging to acquire the precise mathematical models that are necessary for these work [18]. Despite not requiring a model, the performance of fixed-rule FLCs degrades as a result of drifting system parameters, and they do not have an automatic adaptation mechanism. Instead, then focusing on both steady-state and transient performance, most current systems only handle one [17].

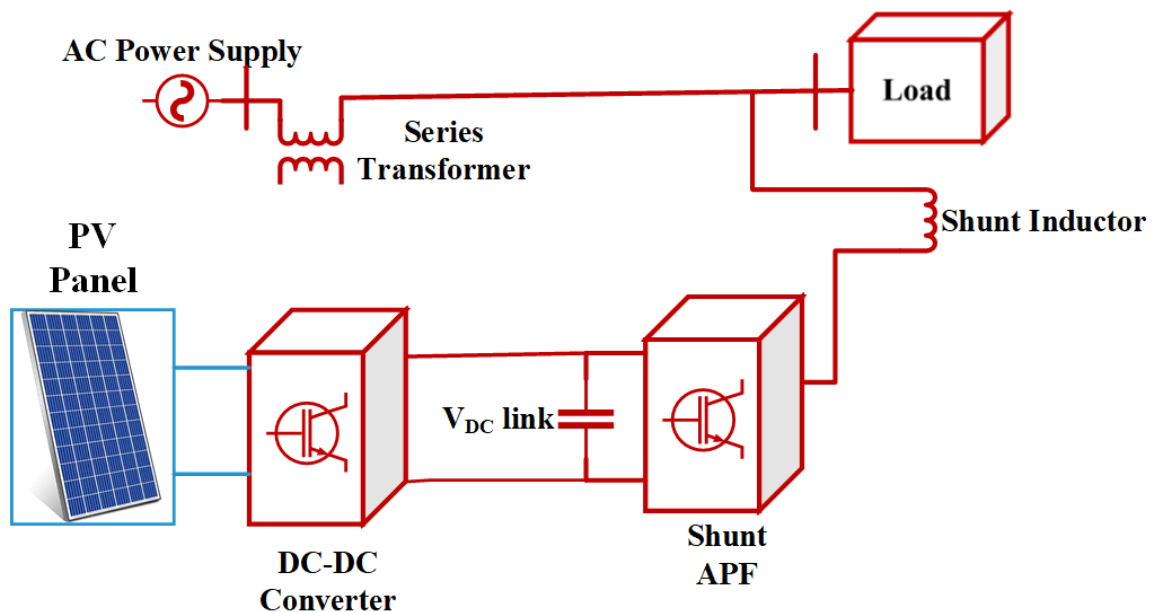


Figure 1. Block diagram of Solar Fed Shunt Active Power Filter

## 2. METHODOLOGY MATHEMATICAL MODELLING AND SYSTEM CONFIGURATION

### 2.1. Shunt APF

Figure 2 presents a block design of the shunt converter. Rectify reactive power and eliminate current harmonics via shunt converters. Shunt Converters supply or absorb power for the DC-Link Capacitor's series converter. A Shunt Converter converts DC-Link-Power-Demand from Series-Converters to AC to enable their operation [43]-[48]. Shunt converters adjust load power consumption via shunt inductance. The  $p - q$  theory uses Clark's Transformation to convert electrical variables from a-b-c coordinates to  $\alpha - \beta$  dimensions. Electrical values are given in  $\alpha - \beta$  coordinates using (1) and (2).

$$\begin{pmatrix} v_{\alpha\_load} \\ v_{\beta\_load} \end{pmatrix} = \sqrt{\frac{2}{3}} \begin{pmatrix} 1 & -\frac{1}{2} & -\frac{1}{2} \\ 0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \end{pmatrix} \begin{pmatrix} v_{a\_load} \\ v_{b\_load} \\ v_{c\_load} \end{pmatrix} \quad (1)$$

$$\begin{pmatrix} i_{\alpha\_load} \\ i_{\beta\_load} \end{pmatrix} = \sqrt{\frac{2}{3}} \begin{pmatrix} 1 & -\frac{1}{2} & -\frac{1}{2} \\ 0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \end{pmatrix} \begin{pmatrix} i_{a\_load} \\ i_{b\_load} \\ i_{c\_load} \end{pmatrix} \quad (2)$$

From (3) and (4), one can calculate the real and reactive power by considering the current and voltage at any point in the coordinates  $\alpha - \beta$ .

$$p_{load}(t) = v_{\alpha\_load}(t)i_{\alpha\_load}(t) + v_{\beta\_load}(t)i_{\beta\_load}(t) \quad (3)$$

$$q_{load}(t) = -v_{\alpha\_load}(t)i_{\beta\_load}(t) + v_{\beta\_load}(t)i_{\alpha\_load}(t) \quad (4)$$

Similar to the Synchronous Reference Frame Theory, the  $p - q$  theory comprises a standard component and an oscillatory factor pertaining to actual and reactive power, as delineated in (5) and (6).

$$p_{load} = \widetilde{p_{ac\_load}} + \overline{p_{dc\_load}} \quad (5)$$

$$q_{load} = \widetilde{q_{ac\_load}} + \overline{q_{dc\_load}} \quad (6)$$

The reference current that is created can be transformed from  $\alpha - \beta$  coordinates to  $a - b - c$  coordinates using (7).

$$\begin{pmatrix} i_{a\_load}^* \\ i_{b\_load}^* \\ i_{c\_load}^* \end{pmatrix} = \sqrt{\frac{2}{3}} \begin{pmatrix} 1 & -\frac{1}{2} & -\frac{1}{2} \\ 0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \end{pmatrix} \begin{pmatrix} -i_{o\_load} \\ i_{\alpha\_load}^* \\ i_{\beta\_load}^* \end{pmatrix} \quad (7)$$

The shunt converter must sustain a stable DC connection voltage. The variation in real and reactive power control is determined by the phase angle  $\delta$ . Reference signals can be generated and transmitted to the PWM generator through contrasting the reference current with the load current. The shunt voltage source converter obtains its gating pulses from the PWM generator.

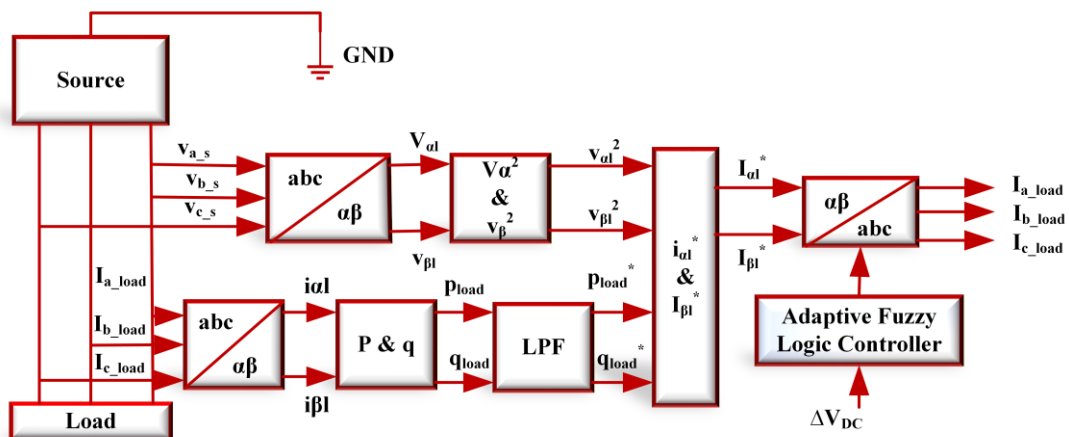


Figure 2. Shunt-APF Configuration

## 2.2. Solar PV System

A PV array is constructed using PV solar cells connected in series and parallel, as shown in Figure 3 for a basic equivalent circuit model. Load current and solar irradiation intensity are the primary determinants of photocurrent, which in turn determines the voltage output of a photovoltaic cell [22]. The series circuit that controls the power output of a solar cell includes a diode, a network of resistors, and an ILGC, as shown in Figure 3 [23][24].

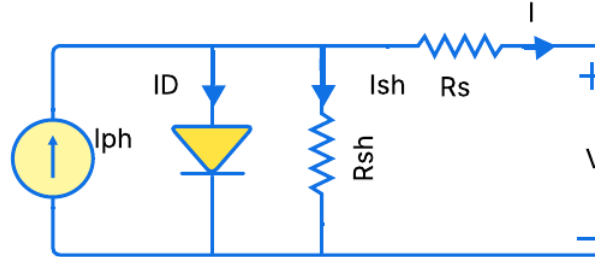


Figure 3. Block diagram of PV cell

Mathematical modelling of solar cell in MATLAB,  $I$  is the output current of PV cell,  $V$  is the output voltage of PV cell,  $I_{ph}$  is the photo generated current,  $I_D$  is the Diode Current,  $I_{sh}$  is the Shunt Current,  $V_{oc}$  is the Open circuit voltage,  $I_{rs}$  is the Diode reverse saturation current ( $I_0$ ),  $I_{csc}$  is the Cell Saturation current at  $T_{rt}$ ,  $I_{scr}$  is the Short circuit current,  $V_{dc}$  is the Diode Voltage,  $R_s$ ,  $R_{sh}$  is the Series and shunt resistances, respectively,  $I_{sh}$  is the Current due to shunt resistance  $C$  is the Elementary charge  $1.6 \times 10^{-19}$ ,  $K$  is the Boltzmann Constant  $1.38 \times 10^{-23}$  J/K,  $\gamma$  is the Idealist Factor,  $T$  is the Cell temperature,  $T_r$  is the Reference temperature,  $K_I$  is the Short circuit current temperature coefficient at  $I_{scr}$ ,  $N_{sc}$  is the number of solar cells in the series in the solar module,  $N_{cp}$  is the number of solar cells in parallel in the solar module. Applying Kirchhoff's current law in the model shown in Figure 3,

$$I = I_{ph} - I_D - I_{sh} \quad (9)$$

$$I = I_{ph} - I_{crs} \{ \exp(AV_D - 1) \} - \frac{V_{dc}}{R_{sh}} \quad (10)$$

$$A = \frac{C}{NYKT} \quad (11)$$

$$V_D = V + IR_s \quad (12)$$

$$I_{crs} = I_{csc} \left[ \frac{T}{T_{rt}} \right]^3 \quad (13)$$

$$I_{ph} = [I_{sc} + K_i(T - T_{rt})] \frac{1}{1000} \quad (14)$$

The current divided through diode is

$$I_D = I_0 \left[ \exp \left( \frac{C(V + IR_s)}{mKT} \right) - 1 \right] \quad (15)$$

Where  $I_0$  is the diode saturation current,  $m$  is the diode quality factor,  $T_c$  is the absolute temperature of cell (K).

$$I = I_{ph} - I_0 \left( \exp \left[ \frac{C(V + IR_s)}{mKT} \right] - 1 \right) - \frac{(V + IR_s)}{R_{sh}} \quad (16)$$

Maximum output of PV panel is as given below. The current at maximum power point  $I_{mpp}$  is

$$I_{mpp} = I_{ph} - I_0 \left( \exp \left[ \frac{C(V_{mpp} + I_{mpp}R_s)}{mKT} \right] - 1 \right) - \frac{(V_{mpp} + I_{mpp}R_s)}{R_{sh}} \quad (17)$$

$I_{mpp}$  is the maximum panel current,  $V_{mpp}$  is the maximum panel voltage,  $P_{max}$  is the maximum power point by PV panel.

$$P_{max} = V_{mpp} \left\{ I_{ph} - I_0 \left( \exp \left[ \frac{C(V_{mpp} + I_{mpp}R_s)}{mKT} \right] - 1 \right) - \frac{(V_{mpp} + I_{mpp}R_s)}{R_{sh}} \right\} \quad (18)$$

The  $V_{out}$  of panel is given as

$$V = N_{sc}(V_{DC} - R_s I) \quad (11)$$

$$I = I_{ph} - I_{dc} - I_{sh} \quad (12)$$

The “Photovoltaic generator (PVG)” or “PV array” is composed of many PV Panels connected in  $N_{sp} - PV$  modules in series,  $N_{pp} - PV$  modules in Parallel panels to indulge desired values of voltage and current.

$$V_{pvm} = N_{sc} * N_{sp} * V_p \quad (19)$$

$$I_{pvm} = N_{pc} * N_{pp} * I_p \quad (20)$$

Where  $V_{pvm}$  and  $I_{pvm}$  are generated output voltage, current at PV array module. Then we have to compute PVarray voltage and current which are  $V_{pva}$ ,  $I_{pva}$  and  $P_{pva}$ .

Where,

$$V_{pva} = V_{pvm} * N_{sc} \quad (21)$$

$$I_{pva} = I_{pvm} * N_{pc} \quad (22)$$

$$P_{pva} = V_{pva} * I_{pva} \quad (23)$$

Solar panels automatically incorporate bypass diodes to regulate the amount of voltage that goes above what is needed. However, the system's price tag will increase as a result of this [19].

### 3. CONTROL METHOD

When dealing with power quality challenges, adaptive fuzzy logic controllers (FLC) are typically preferred over traditional controllers due to their superior ability to manage nonlinear, time-varying, and unpredictable system dynamics. If the system parameters are unpredictable or difficult to model, FLC can be used because it does not require an exact mathematical model but instead operates on linguistic norms [35]. The ability to adjust membership functions and rules in real time allows adaptive FLC to be more flexible and keep performance constant regardless of changes in load or supply. Superior to fixed-parameter PI/PID controllers in handling harmonics, voltage sags/swells, and other unforeseen disturbances; robust to disturbances. Speedier dynamic response-Improves power quality in transient settings by rapidly adjusting control actions without excessive overshoot or steady-state error [36]. For complicated and changeable power quality problems, adaptive fuzzy logic controllers (FLCs) are better than traditional, inflexible controllers because they mix fuzzy logic with real-time self-tuning.

The error ( $V_{dref} - V_{dc}$ ) and the change in error serve as the sources for the FLC, which are inputs to the FLC controller. The FLC is constantly evaluating and computing the inputs, and fuzzy logic rules are used to

optimize the performance of the PI controller parameters on the fly [37]-[42]. Figure 4 displays the Adaptive FLC control diagram. Adaptive FLC inputs might meet PI self-calibration requirements for error, change in error, and output at different intervals. Figure 5 shows the input variables' membership functions, whereas Figure 6 shows the same thing for the output variables. The integral gain  $K_I$  membership function is shown in Figure 7, while the proportional gain  $K_P$  membership function is shown in Figure 8. Figure 8 shows the control strategy flow diagram that was suggested [25][26].

The implementation process of an adaptive controller includes performance input. By assigning recognitions or recompenses to particular control actions that improve present performance, the index gives finest states for constructing the best constraint states through Fuzzy Interface System. If you want your output control signal to work as well as possible, you need to get rid of power loss caused by things like harmonics, voltage distortion, current distortion, and similar issues [27]-[31]. The membership functions (MFs) for all fuzzy variables are negative big (NB), negative medium (NM), negative small (NS), zero (ZE), positive small (PS), positive medium (PM), positive big (PB). To apply the same MFs for these variables as in the previous way, it can expand the FLC's inference table to include the source and load voltages and currents. An FLC rule table is shown in Table 1.

To reduce harmonics in the load current, an Adaptive FLC based on an APF is used. It is possible to approximate the orientation currents by regulating the DC link voltage. The voltage at the point of addition has a reference value. The current state of the error signal monitoring is ensured by FLC, which controls the signal so that the error is always zero. To maintain a constant DC interface voltage, the current regulator adjusts this little active current in response to feedback from the FLC. Figure 4 shows the schematic of the an Adaptive FLC based Shunt APF control system [32]-[36]. To some degree, the projected Adaptive FLC approach reduces effect of outside conflicts and errors. Targeting nonlinear systems with few known or uncertain parameters and disturbances, it combines fuzzy framework qualities with adaptive control tactics, critique linearization methods, and optimum control theory to solve trajectory control problems.

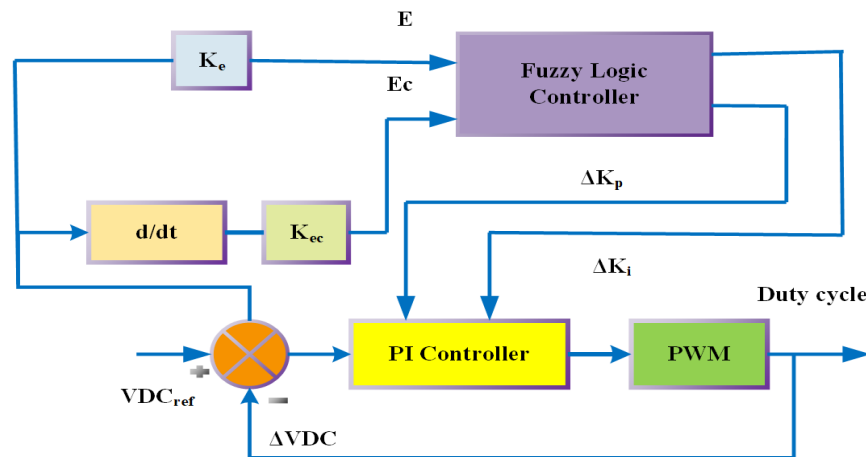


Figure 4. Control block diagram for Adaptive Fuzzy Logic Controller

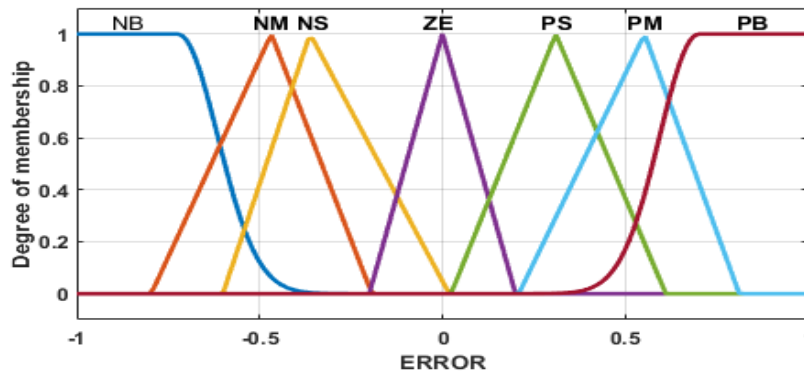


Figure 5. Error MFs

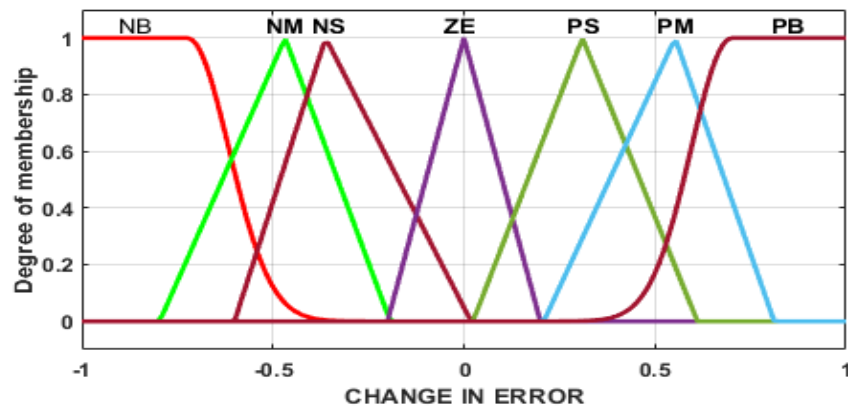


Figure 6. Change in Error MFs

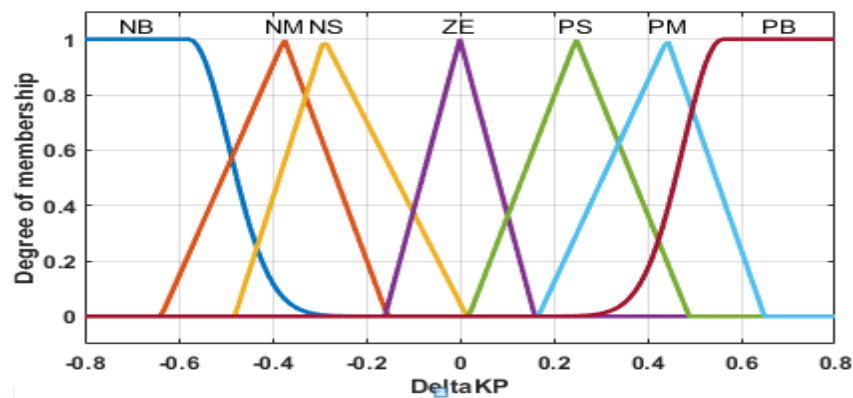
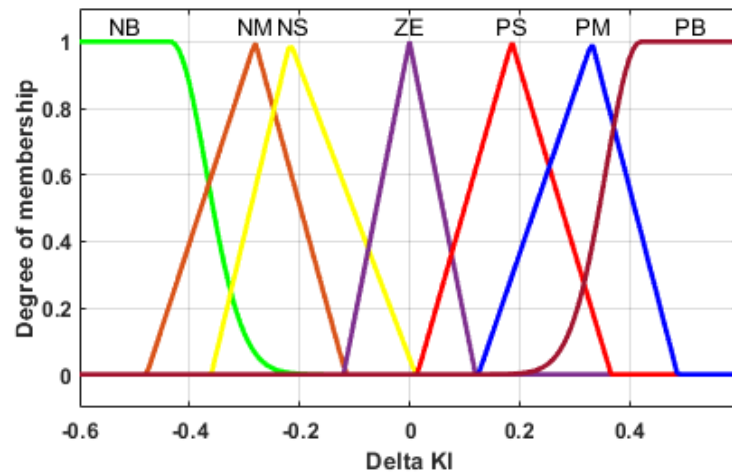
Figure 7.  $\Delta K_p$  MFsFigure 8.  $\Delta K_i$  MFs

Table 1. Rule table for FLC

Rule Table	Change of Error ( $\Delta e$ )						
	NB	NM	NS	ZE	PS	PM	PB
Error (e)	NB	NB	NB	NB	NM	NS	ZE
	NM	NB	NB	NM	NS	ZE	PS
	NS	NB	NB	NS	ZE	PS	PM
	ZE	NB	NM	NS	ZE	PS	PM
	PS	NM	NS	ZE	PS	PM	PB
	PM	NS	ZE	PS	PM	PB	PB
	PB	ZE	PS	PM	PB	PB	PB



#### 4. RESULT AND DISCUSSION

Figure 9 and Figure 10 Current Compensation with FLC and Adaptive FLC, respectively. The suggested adaptive controller stabilizes the source current, resulting in a sinusoidal waveform and minimized fluctuations. The simulation results for  $V_s$  and  $I_s$  during distortion after the deployment of Adaptive FLC are presented in Figure 11 and Figure 12. Figure 11 illustrates the Source Voltage and Source Current with Adaptive FLC, while Figure 12 illustrates the Voltage Source and Current Source with FLC. It examines the Adaptive FLC, which maintains a steady source voltage magnitude compared to FLC, while also reducing source current distortions. Figure 13 and Figure 14 present the simulation results for  $V_L$  and  $I_L$  during distortion subsequent to the introduction of Adaptive FLC. Figure 13 illustrates the voltage ( $V_L$ ) and current ( $I_L$ ) with fuzzy logic control (FLC), whereas Figure 14 presents the voltage ( $V_L$ ) and current ( $I_L$ ) with Adaptive fuzzy logic control. It examines the Adaptive FLC, which maintains a steady voltage magnitude compared to FLC, while also reducing load current distortions. Figure 15 to Figure 22 illustrate total harmonic distortion (THD) for source and load currents, source and load voltages, respectively.

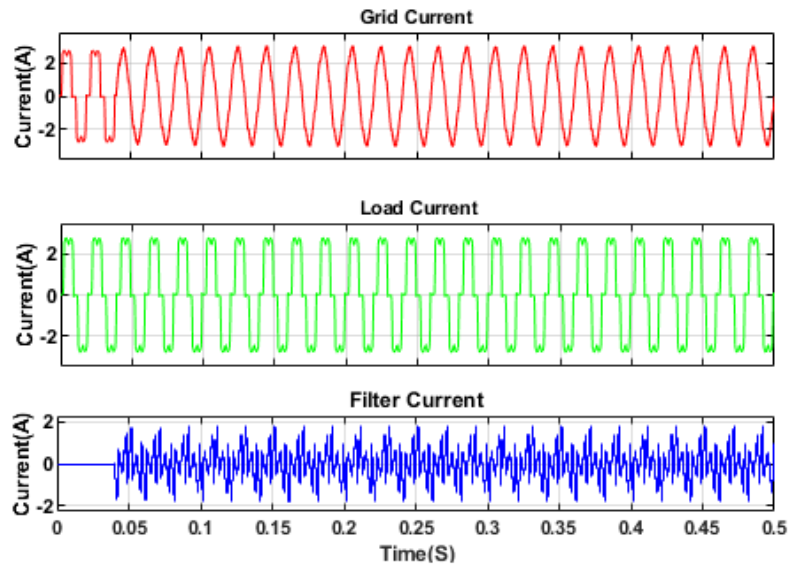


Figure 9. Simulation result Current of Compensation with FLC

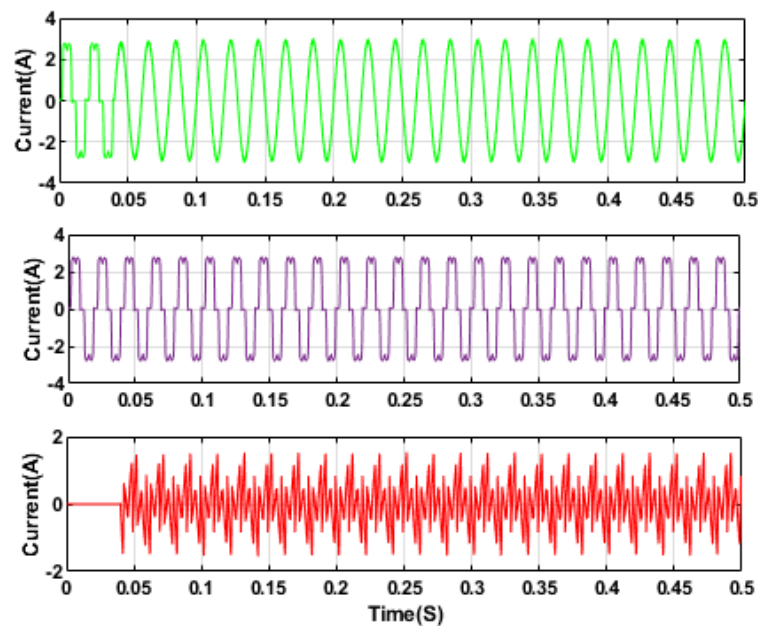
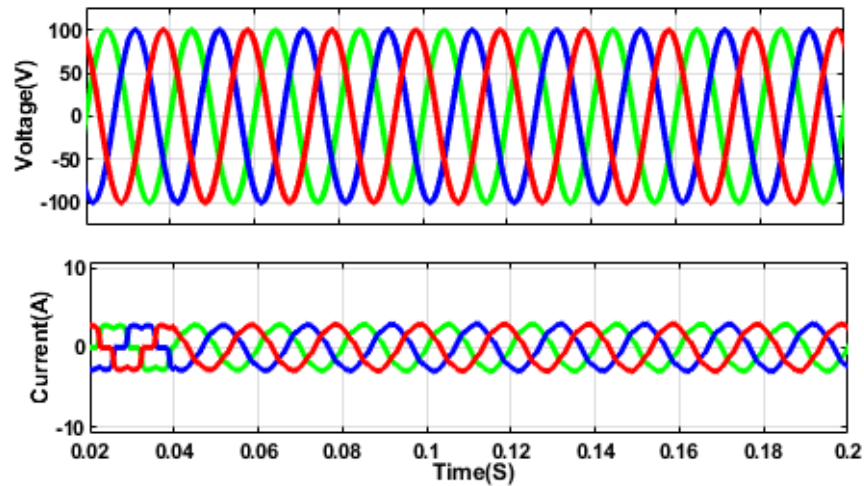
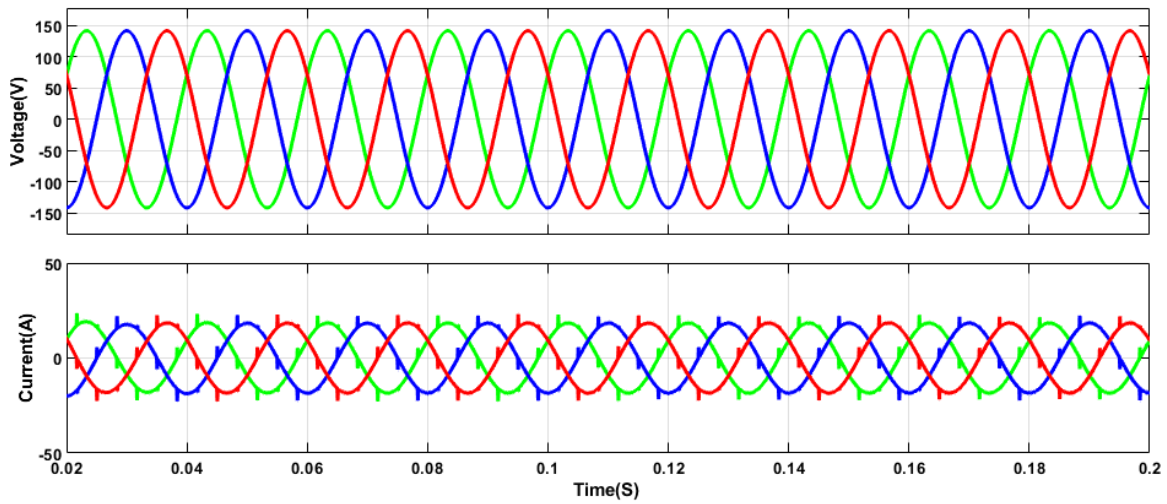
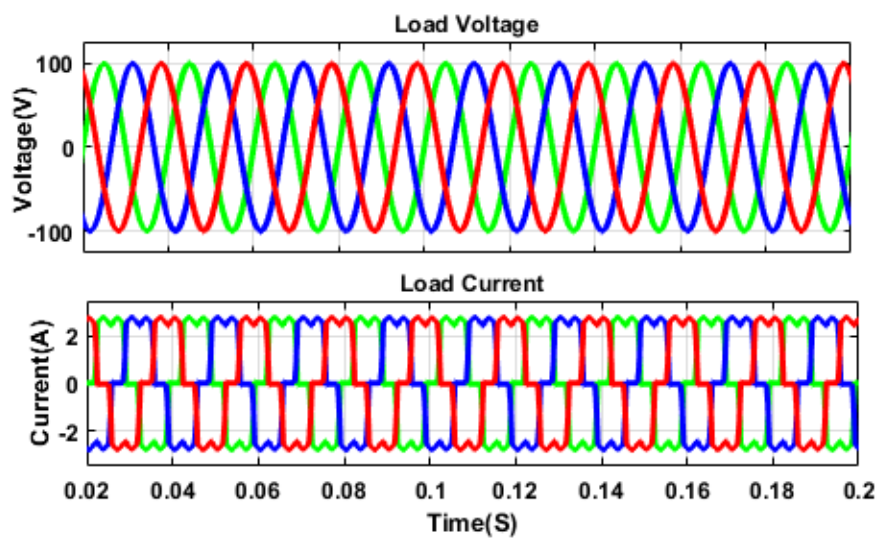


Figure 10. Simulation result of Current Compensation with Adaptive FLC



Figure 11. Result of  $V_s$  and  $I_s$  with Adaptive FLCFigure 12. Result of  $V_s$  and  $I_s$  with FLCFigure 13. Simulation result of  $V_L$  and  $I_L$  with FLC

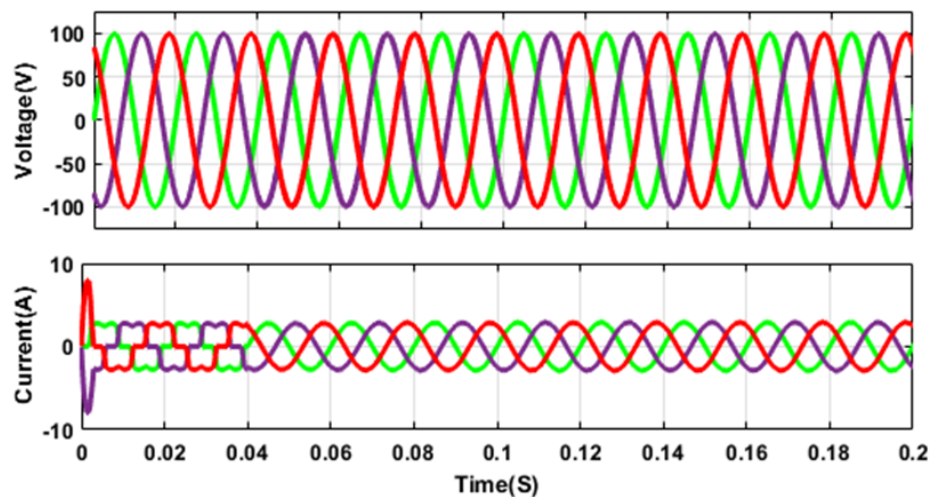
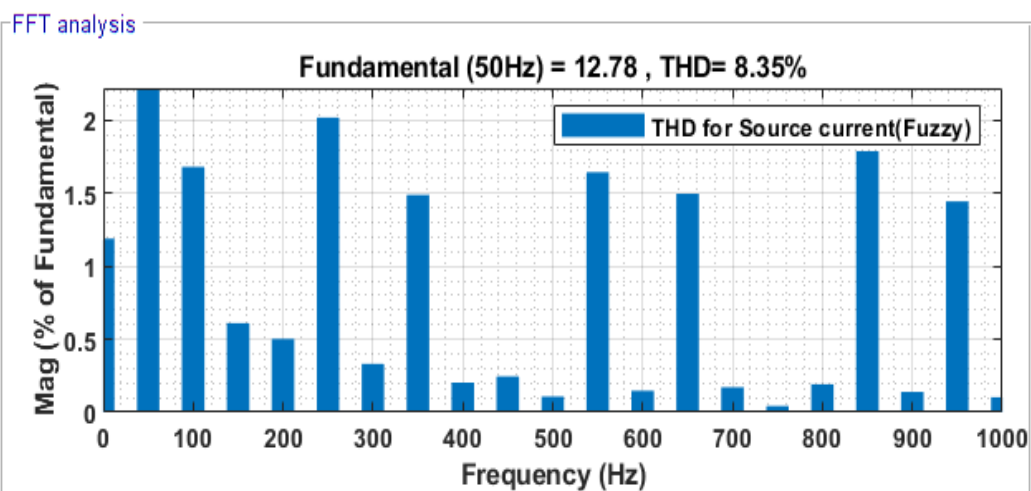
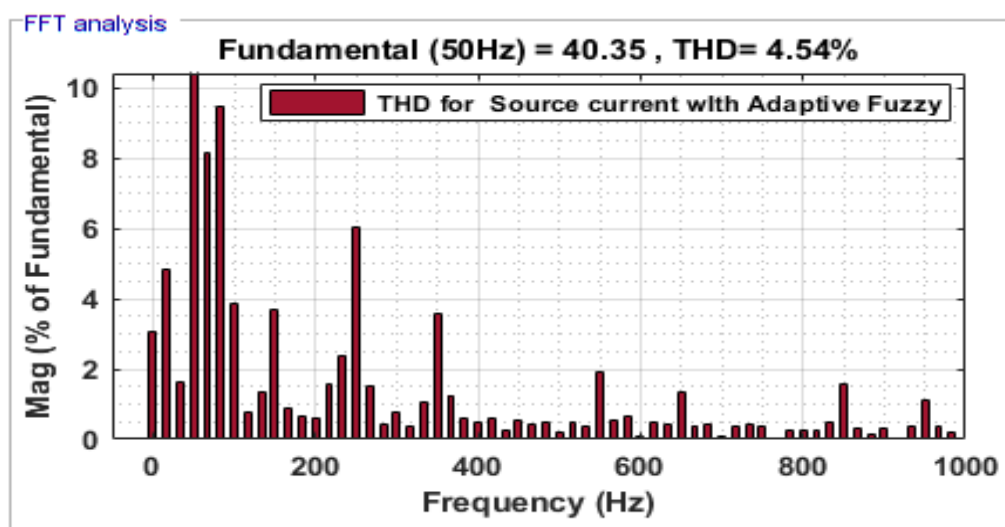
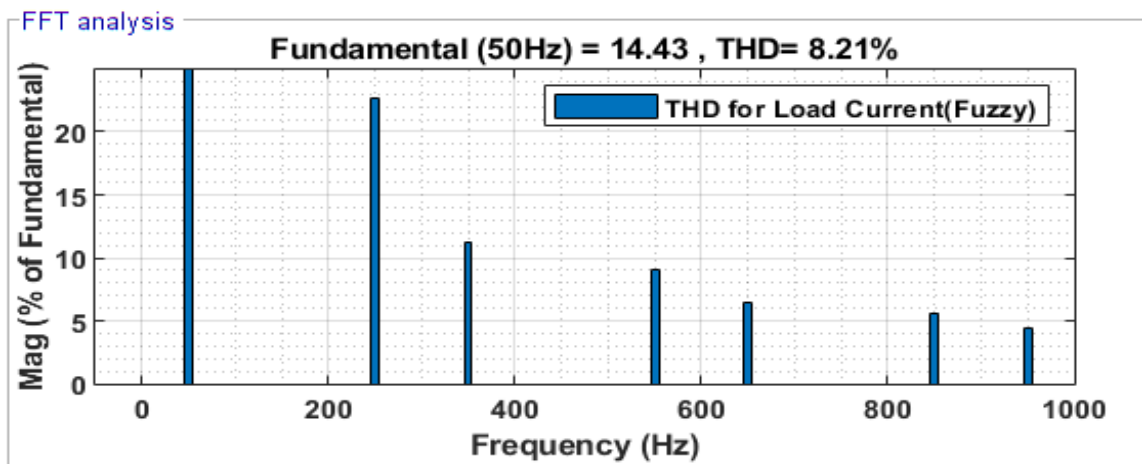
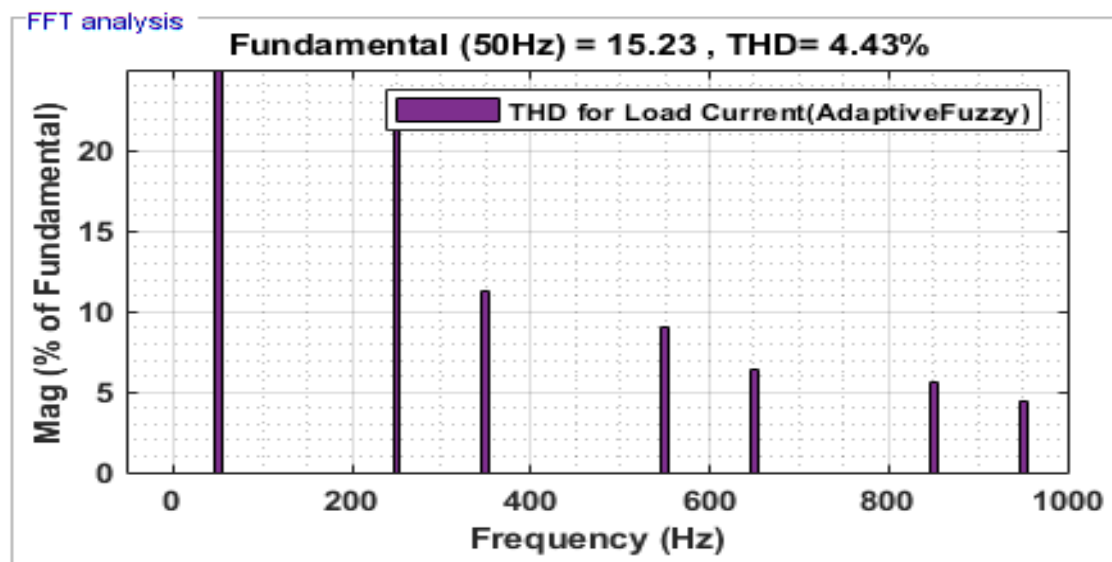
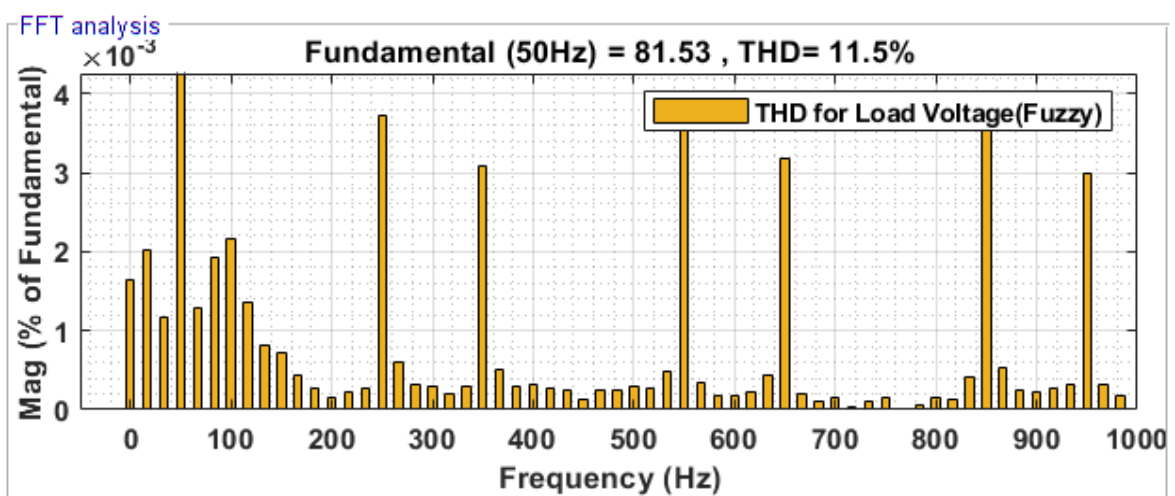


Figure 14. Simulation result of Load Voltage and Load Current with Adaptive FLC

Figure 15. THD for  $I_s$  with FLCFigure 16. THD for  $I_s$  with Adaptive FLC

Figure 17. THD for  $I_L$  with FLCFigure 18. THD for  $I_L$  with Adaptive FLCFigure 19. THD for  $V_L$  with FLC

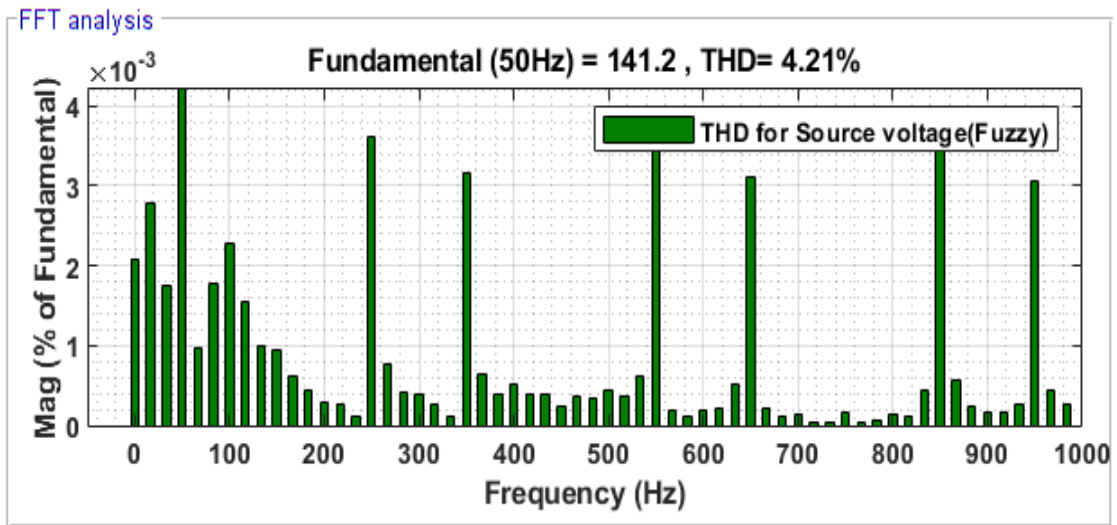
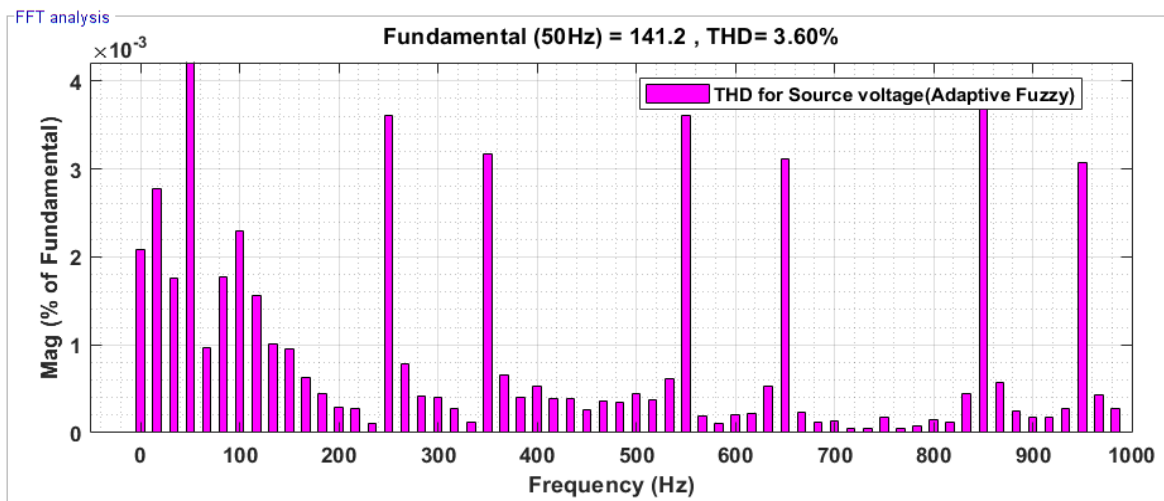
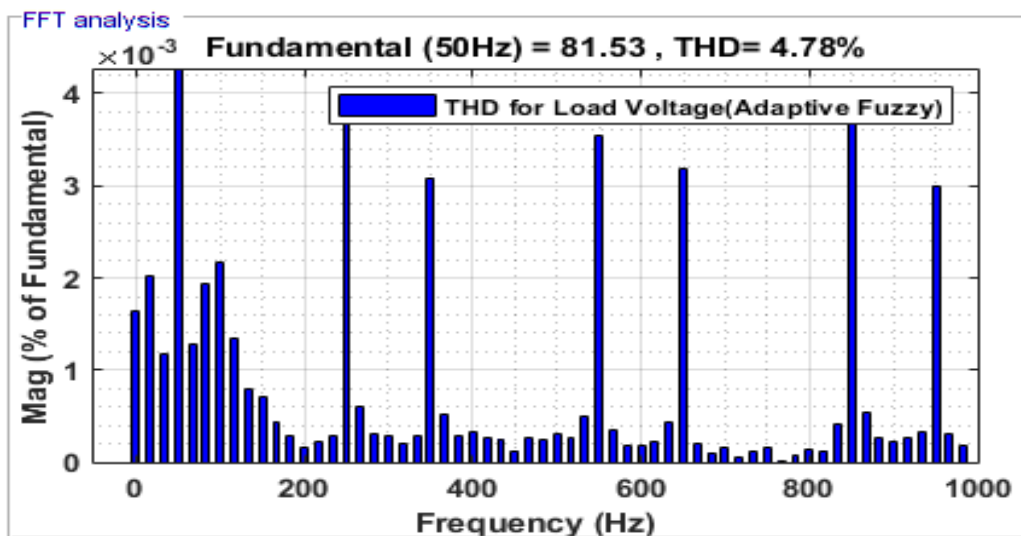
Figure 20. THD for  $V_S$  with FLCFigure 21. THD for  $V_S$  with Adaptive FLCFigure 22. THD for  $V_L$  with Adaptive FLC

Table 2. Comparison of THD values

Control Methods	% THD Values			
	Source Current	Source Voltage	Load Current	Load Voltage
PV fed Shunt APF without PI	18.8%	14.8%	24%	23.4%
PV fed Shunt APF with PI	16.6%	6.1%	10.3%	15.1%
PV fed Shunt APF with FLC	8.35%	4.21%	8.21%	11.5%
PV fed Shunt APF with Adaptive FLC	4.54%	3.60%	4.43%	4.78%

## 5. CONCLUSIONS

Adaptive FLC based Shunt APF is proposed in this Paper to tackle power quality difficulties and VDC-Link regulation, two of the most pressing problems in the power quality industry. The MATLAB/Simulink model is built and the simulation results are evaluated to determine how the shunt APF's two controllers, the FLC and the Adaptive FLC, work. Every controller has its own THD value, which is then compared with the others. Findings demonstrate that 3.60% for source voltage and 4.54 % for source current THD when an Adaptive FLC is employed. One more proof that this controller's compensation for all parameters works. Thus, among the alternatives, the adaptive FLC offers the best performance. Among the many advantages of the proposed controller are the following: Voltage distortion was used to provide steady voltage regulation. There is a considerable improvement in power supply losses and VSI compared to the earlier method. There are a lot of Power Q problems that can be solved by the current approach using Shunt APF

## DECLARATION

### Author Contribution

All authors contributed equally to the main contributor to this paper. All authors read and approved the final paper.

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### Conflicts of Interest

No conflict of interest.

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